$$\begin{array}{c} ANSWER \quad SHEET\\ LAB 4 \end{array}$$

$$\begin{array}{c} F_{Xersize} \\ \hline \\ F_{Xersize} \\ \hline \\ F_{X} \\ F_{X} \\ \hline \\ F_{X} \\ F_{X$$

Exercise /

 $B) FOR X, + X_z = 40 \, km$ · FIND i $X_1 + X_2 = 40$ km = (H-TH) tan i + (TH) tan j = (H-TH)tanit TH tan (sin' (B sin i)) i= 83.9° · FIND RAY PARAMETER $\frac{P = \sin i}{\beta_2} = \frac{\sin (83.7^\circ)}{3.5 \text{ km/s}} = 0.2.84 \text{ s/km}$ · FIND TRAVEL TIME $t = P(x_1 + x_2) + TH \eta_1 + (H - TH) \eta_2$ = (0.284 s/km) (40 km) + (4 km) (0.412 s/km) + (8-4) (0.030 s/km) 7,=0.4115 = 13,13 s $\eta_2 = 0.0305$ ·FIND TRANSMISSION COEFFICIENT $T_{21} = \frac{2 M_2 \eta_2}{M_1 \eta_1 + M_2 \eta_2}$ 2(2.6 9/cc) 3.5 km/s) (0.030 s/km) (29/cc) 2km/s) (0.412 s/km) + (2.6 9/cc) 3.5 km/s) (0.030 s/km) F10.45

Thus at grazing incidence the amplitude of the direct arrival is greatly roduced due to energy reflecting downword at the intertace. On attenuation curves this would result in greater them 'Ir attenuation of the direct phase.

Exersize 2

$$\frac{x}{P_{1} = \sqrt{\frac{x}{\beta_{1}^{2}} - \rho^{2}}} = \frac{\cos j}{\beta_{1}} = \frac{1}{\beta_{1}^{2}} - \rho^{2}} = \frac{\cos j}{\beta_{1}} = \frac{1}{\beta_{1}^{2}} - \rho^{2}} = \frac{\cos j}{\beta_{1}} = \frac{1}{\beta_{1}^{2}} - \rho^{2}} = \frac{\cos j}{\beta_{1}} = \frac{1}{\beta_{2}} - \rho^{2}} = \frac{\cos j}{\beta_{2}} = \frac{1}{\beta_{2}} + \frac{1}{\beta_{2}} - \rho^{2}} = \frac{\cos j}{\beta_{2}} = \frac{1}{\beta_{2}} + \frac{1}{\beta_{2}} - \rho^{2}} = \frac{\cos j}{\beta_{2}} = \frac{1}{\beta_{2}} + \frac{1}{\beta_{2}} - \rho^{2}} = \frac{\cos j}{\beta_{2}} = \frac{1}{\beta_{2}} + \frac{1}{\beta_{2}} - \rho^{2}} = \frac{\cos j}{\beta_{2}} + \frac{1}{\beta_{2}} - \rho^{2}} = \frac{\cos j}{\beta_{2}} + \frac{1}{\beta_{2}} + \frac{1}{\beta_{2}} - \rho^{2}} = \frac{\cos j}{\beta_{2}} + \frac{1}{\beta_{2}} + \frac{$$

The amplitude is only 1/3 of the amplitude of the direct arrival

B)
$$F_{OR} = 40 \text{ km}$$

 $40 \text{ km} = (\text{H-TH}) \tan i + 3 \text{TH} \tan j$
 $40 \text{ km} = (\text{H-TH}) \tan i + 3 \text{TH} \tan (\sin^{-1}(\frac{B_{1}}{R_{2}} \sin i))$
 $i = 82.8^{\circ}$
• FIND $R_{AY} P_{ARAMETER}$
 $P = \frac{\sin i}{B_{2}} = 0.283 \text{ s/km}$
• FIND $T_{RAYEL} TIME$
 $t = PX + \eta_{2}(H-TH) + 3 \text{TH} \eta_{1}$
 $= 16.4 \text{ s}$
• FIND $T_{OTAL} T = 4NO R$ RESPONSE
 $T_{21} = \frac{2.42}{4.\eta_{1}} \frac{\eta_{2}}{\eta_{2}} R_{10} = 1$ $R_{12} = \frac{4.\eta_{1} - 42.\eta_{2}}{42.\eta_{2}} \frac{\eta_{2}}{\eta_{2}} + 4.\eta_{1}},$
 $T_{OTAL} = T_{24} \cdot R_{10} \cdot R_{12} = (0.513)(1X0.487)$
 $= 0.25$ The multiple is a little more from 12 the mo

Exercise 3

$$\frac{x_{1}}{x_{2}}, \frac{x_{2}}{x_{2}}, \frac{x_{2}}$$

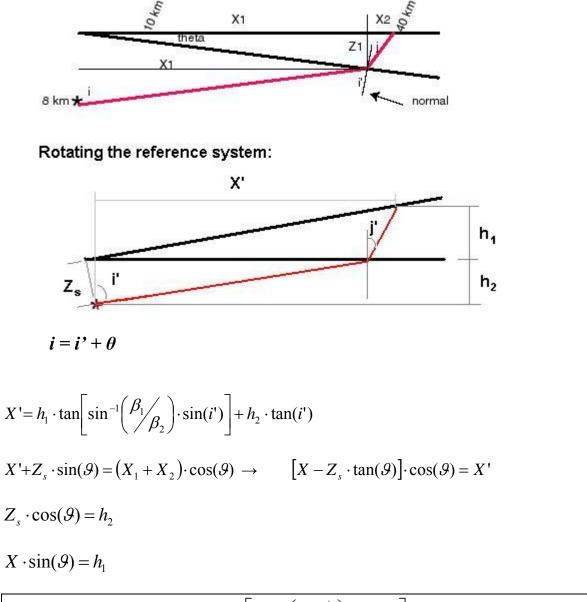
 $X_2 = Z_1 \tan(j + \phi)$ $x_2 = x_1 \tan - e \tan (i + e)$ $\begin{aligned} X_{2} &= X_{i} \tan \phi \tan \left(\sin^{-1} \left(\frac{\beta_{i}}{\beta_{2}} \sin(i - \phi) \right) + \phi \right) \\ X_{2} &= \left(\frac{h \cdot \tan i}{1 + \tan(i) \tan(\phi)} \right) \tan \phi \tan \left(\sin^{-1} \left(\frac{\beta_{i}}{\beta_{2}} \sin(i - \phi) \right) + \phi \right) \end{aligned}$ THEREFORE $X_{1} + X_{2} = \frac{h \cdot tan i}{1 + tan(i)tan(\phi)} \left(1 + tan - \phi \cdot tan(sin'(\frac{B_{1}}{B_{2}}sin(i-\phi)) + \phi \cdot tan(sin'(\frac{B_{1}}{B_{2}}sin(i-\phi))) + \phi \cdot tan(sin'(\frac{B_{1}}{B_{2}}sin(i-\phi)) + \phi \cdot tan(sin'(\frac{B_{1}}{B_{2}}sin(i-\phi))) + \phi \cdot tan(sin'(\frac{B_{1}}{B_{2}}sin(\frac{B_{1}}{B_{2}}sin(i-\phi))) + \phi \cdot tan(sin'(\frac{B_{1}}{B_{2}}sin$ · Assuming == 5° and X, + Xz = 10 km, FIND i Using the above expression and iterating over i i= 53.0° · FIND RAY PARAMETER (10 km) $P = \frac{\sin t}{B_{-}} = 0.228 \text{ s/km}$ · FIND LOCAL RAY PARAMETER (IOKm) $P_{L} = \frac{\sin(i-\phi)}{R_{L}} = 0.212 \text{ s/km}$ · FIND TRAVEL TIME (10 km) $t = P(x_1 + x_2) + \eta_2(h - Z_1) + \eta_1^* Z_1 = 3.9$ 7/2= 0.171 where $7/^* = \int \frac{1}{8^2} - P_2^2 = 7/1.$ $\sqrt{\frac{1}{3\frac{5}{2}} - P_{L}^{2}} = \frac{7}{2L}$

Exercise 3

TRAVEL TIME MAY ALSO BE FOUND BY $\frac{\sqrt{X_{1}^{2} + (h - Z_{1})^{2}}}{4} + \frac{\sqrt{(X_{1} + X_{2} - X_{1})^{2} + Z_{1}^{2}}}{3.9 \text{ s}}$ βı where Z_i = h.tani tano tano · TRANSMISSON COEFFICIENT (IOKM) 711 = 0.453 $T_{21} = \frac{2 M_2 \eta_{2L}}{M_1 \eta_{1L} + M_2 \eta_{2L}} = 1.254 \quad \eta_{1L} = 0.453$ increase of 14%. · FOR X, + X, = 40 km i= 82.8° 7/12=0.415 P= 0.2.83 s/km 7/22=0.06 P,= 0.2.79 s/km $7_2 = 0.035$ t = 12.9 sT2= 0.735 increase of 60%. Thus the dipping structure allows for more efficient transmission.

Dipping structure greatly enhances the transmission. Similarly, the R12 reflection can be found to be greater. This type of structure traps energy !

Alternatively, the solution for the ray can be found by rotating the reference system, as shown in the figures bellow:



$$X_1 + X_2 = \frac{\left(X_1 + X_2\right) \cdot \sin(\vartheta) \cdot \tan\left[\sin^{-1}\left(\frac{\beta_1}{\beta_2}\right) \cdot \sin(i')\right] + Z_s \cdot \cos(\vartheta) \cdot \tan(i')}{\cos(\vartheta)} + Z_s \cdot \tan(\theta)$$

For
$$\theta = 5^{\circ}$$
, $Z_s = 8$ km, $\beta_1 = 2$, $\beta_2 = 3.5$
 $X = 10 \rightarrow i' = 48.02^{\circ} \rightarrow i = 53.02^{\circ} \rightarrow X' = 9.26$ km
 $X = 40 \rightarrow i' = 77.78^{\circ} \rightarrow i = 82.78^{\circ} \rightarrow X' = 39.15$ km